

▷ 1391 Corporate Drive | Suite 203 | McHenry, IL 60050 Main 815.385.1778 + Fax 815.385.1781 ▷ HRGREEN.COM

January 5th, 2024

To: City Naperville 400 S. Eagle Street Naperville, IL 60540

From: Joseph Vavrina, P.E.

Subject: Stormwater Memo Chick-fil-A – Naperville, IL Job #: 2302569

Background

Chick-fil-A (CFA) is proposing the construction of an approximate 5,000 square foot free-standing restaurant, drivethru lane, parking facilities, and associated utilities located within the Iroquois Center Development in the City of Naperville (1163 E. Ogden Avenue). This project is more generally located along the north side of Ogden Avenue between Iroquois Avenue and East Avenue. The proposed stormwater management improvements have been designed in accordance with the requirements of the City of Naperville.

Existing Conditions

The subject CFA project area is located on the south side of the Iroquois Center Development. The project area currently encompasses part of a multi-tenant retail building and parking lot that will be razed as part of this project. The site is bordered by the multi-tenant building to the west, Staples parking lot to the south, parking lot & access drive to the north, and Ogden Avenue to the east. The proposed lease parcel is approximately 1.70 acres (73,927 sq. ft.) in size. In the existing condition, the impervious and pervious areas within the lease parcel are calculated to be 68,126 square feet and 5,801 square feet respectively, resulting in the site to be 92% impervious.

The subject site is currently tributary to the storm sewer system for the Iroquois Center Development. This storm sewer system drains to the west of the CFA site to a regional detention basin. Per previous design plans for the center, the regional basin was designed with a high water level (HWL) of 766.00. In addition to the basin, it was discovered that stormwater detention for the center is also provided via storm sewer and parking lot surface storage.

Per the ALTA survey, pipe and parking lot detention storage is currently provided within the CFA project site. The existing storage with the site (up to an elevation of 766.00) has been calculated to be approximately 5,374 cubic feet (0.123 ac-ft). The CFA development will need to replace this detention storage as part of the proposed improvements. All existing detention storage calculations and exhibits have been included with this report.

Proposed Conditions

The proposed improvements to the site consist of the construction of the Chick-fil-A restaurant, drive-thru lane, parking facilities, and the installation of underground utilities. In the proposed condition, the impervious and pervious areas within the subject parcel are calculated to be 56,232 square feet and 17,695 square feet respectively, resulting in the site to be 76% impervious. The proposed improvements will be decreasing the impervious coverage by approximately 11,894 square feet from the existing condition.



As noted in the existing conditions section, the CFA development will be required to provide onsite stormwater detention for the pipe & parking lot storage that will be taken away. The storm system has been oversized (up to 36 inch diameter pipe) to provide the required storage. The total storage being provided has been calculated to be 5,720 cubic feet (0.131 ac-ft).

The CFA site has been designed to capture and convey stormwater via an onsite storm sewer system. Catch basin structures have been introduced around the site to capture runoff from the various drainage areas and convey stormwater to the existing Iroquois Cetner storm sewer system. The onsite drainage areas for each storm structure have been delineated on the Proposed Drainage Plan (PDP).

The new storm sewer installed as part of the CFA improvements will be able to convey the 2-year event due to existing storm sewer size constraints. The system can convey the 2-year event without the HGL exceeding the proposed rim elevations. The storm sewer was modeled utilizing Hydraflow Storm Sewers for AutoCAD Civil3D, 2023. Illinois State Water Survey (Bulletin 75) rainfall intensities for the 2-year event were utilized in all calculations. Per the model, the proposed flow within pipes ST-2 and ST-4 exceeds the capacity but these pipes are both existing and will remain in place. Onsite drainage areas were defined for each individual storm sewer catch basin. These drainage areas can be seen on the PDP and are also noted in the Rational "C" Calculation table included in this memo. The times of concentration used in calculation for each drainage area were assumed to be 5 minutes due to short onsite flow paths. The Hydraflow model was also utilized to calculate the HGL of the storm sewers, verifying that the HGL is below the rim elevations of the storm structures. The Hydraflow model and inlet capacity calculations have been included in this report.

The CFA site has been designed to provide overland flood routes throughout the parking lot and drive-thru lane to direct water away from the CFA building. The overland flood path ultimately reaches the west side of the site where it is directed to the regional basin for the overall development. The overland flood route through the CFA site has been shown via bold arrows on the Grading Plan (C-300).

Erosion Control

Installation of sediment and erosion control measures will be placed prior to the start of construction. Inlet protection baskets and silt fence are planned to be installed to control erosion and silt displacement until vegetation is established.



RATIONAL METHOD "C" CALCULATION

Project #:	2302569						
Project:	CHICK-FIL-A			Ву	NHL	Date	11/6/2023
Location:	NAPERVILLE, IL			Checked		Date	
				Revised	NHL	Date	1/4/2024
					-		
BASIN	AREA	AREA	AREA	%PAVED	%GRASS	RUNOFF	AREA
NO.	(SQ-FT)	PAVED	GRASS	0.95	0.35	"C"	(acres)
CFA PROJECT AREA							
EXISTING CONDITION	73,927	68,126	5,801	92%	8%	0.90	1.70
PROPOSED CONDITION	73,927	56,232	17,695	76%	24%	0.81	1.70
PROPOSED DRAINAGE AREAS							
PR-DA-1	6,343	6,343	0	100%	0%	0.95	0.15
PR-DA-2	5,100	4,730	370	93%	7%	0.91	0.12
PR-DA-3	2,587	2,318	269	90%	10%	0.89	0.06
PR-DA-4	3,598	2,703	895	75%	25%	0.80	0.08
PR-DA-5	4,485	4,415	70	98%	2%	0.94	0.10
PR-DA-5A (BUILDING)	5,226	5,226	0	100%	0%	0.95	0.12
PR-DA-6	6,523	5,853	670	90%	10%	0.89	0.15
PR-DA-7	7,689	6,345	1,344	83%	17%	0.85	0.18
PR-DA-8	2,200	2,200	0	100%	0%	0.95	0.05
PR-DA-9	6,788	5,841	947	86%	14%	0.87	0.16
PR-DA-10	4,438	2,114	2,324	48%	52%	0.64	0.10
PR-DA-11	9,168	6,147	3,021	67%	33%	0.75	0.21
PR-DA-12	9,125	1,071	8,054	12%	88%	0.42	0.21
PR-DA-13	655	655	0	100%	0%	0.95	0.02



RATIONAL METHOD "C" CALCULATION

Project #: Project: Location:	2302569 CHICK-FIL-A NAPERVILLE, IL			By Checked	Date 11/6/2023 Date		
				Revised		Date	
BASIN	AREA	AREA	AREA	%PAVED	%GRASS	RUNOFF	AREA
NO.	(SQ-FT)	PAVED	GRASS	0.95	0.35	"C"	(acres)
PROPOSED DRAINAGE AREAS OFF-SITE							
PR-DA-5B	42,539	35,539	7,000	84%	16%	0.85	0.98
PR-DA-5C	52,974	51,213	1,761	97%	3%	0.93	1.22



INLET CAPACITIES

Project #:	2302569	By <mark>N</mark>	IHL Date	11/8/2023
Project:	CHICK-FIL-A	Checked	Date	
Location:	NAPERVILLE, IL	Revised <mark>N</mark>	IHL Date	1/4/2024

CURB INLETS

Structure Number	Frame and Grate	Flow 10-Year (CFS)	Water Depth (ft) Required to Accommodate Flow	Ponding Depth (ft) Provided
ST 3	R-3235 TY A	0.98	0.20	0.50
ST 5	R-2504 TY D	0.79	0.15	0.50
ST 9	R-3235 TY A	0.39	0.10	0.50
ST 11	R-3235 TY A	0.49	0.15	0.50
ST 13	R-3235 TY A	1.57	0.30	0.50
ST 21	R-3235 TY A	0.99	0.20	0.50
ST 25	R-3235 TY A	1.11	0.20	0.50
ST 27	R-3235 TY A	0.36	0.10	0.35
ST 23	R-3235 TY A	1.00	0.20	0.50
ST 34	R-3235 TY A	0.52	0.15	0.40
ST 36	R-3235 TY A	1.18	0.20	0.50

Inlet Capacities per IDOT Design Manual

Neenah R-3235

Type A Grate

0.9 = Free open area of grate (sq. ft.)

4.5 = Weir Perimeter of grate (ft.)

	Capaci				
	Weir	Orifice	Net	Weir/Orifice	Flow Type
Ponding	Equation	Equation	Capacity	ratio	
0.05	0.15	0.97	0.15	0.16	Weir Flow
0.10	0.43	1.37	0.43	0.31	Weir Flow
0.15	0.78	1.68	0.78	0.47	Weir Flow
0.17	0.95	1.79	0.95	0.53	Weir Flow
0.20	1.21	1.94	1.21	0.62	Weir Flow
0.25	1.69	2.17	1.54	0.78	Transition Flow
0.30	2.22	2.37	1.84	0.93	Transition Flow
0.35	2.80	2.56	2.14	1.09	Transition Flow
0.40	3.42	2.74	2.46	1.25	Transition Flow
0.45	4.08	2.91	2.79	1.40	Transition Flow
0.50	4.77	3.06	3.06	1.56	Orifice Flow
0.55	5.51	3.21	3.21	1.71	Orifice Flow
0.60	6.27	3.36	3.36	1.87	Orifice Flow
0.65	7.07	3.49	3.49	2.02	Orifice Flow
0.70	7.91	3.63	3.63	2.18	Orifice Flow
0.75	8.77	3.75	3.75	2.34	Orifice Flow
0.85	10.58	4.00	4.00	2.65	Orifice Flow
1.00	13.50	4.33	4.33	3.12	Orifice Flow
1.25	18.87	4.84	4.84	3.89	Orifice Flow
1.50	24.80	5.31	5.31	4.67	Orifice Flow
1.75	31.25	5.73	5.73	5.45	Orifice Flow
2.00	38.18	6.13	6.13	6.23	Orifice Flow
2.25	45.56	6.50	6.50	7.01	Orifice Flow
2.50	53.36	6.85	6.85	7.79	Orifice Flow
2.75	61.56	7.19	7.19	8.57	Orifice Flow
3.00	70.15	7.51	7.51	9.35	Orifice Flow
3.25	79.10	7.81	7.81	10.12	Orifice Flow
3.50	88.40	8.11	8.11	10.90	Orifice Flow
3.75	98.03	8.39	8.39	11.68	Orifice Flow
4.00	108.00	8.67	8.67	12.46	Orifice Flow
4.25	118.28	8.93	8.93	13.24	Orifice Flow
4.50	128.87	9.19	9.19	14.02	Orifice Flow

Notes:

Equations used Q=0.6A(2gh)^0.5 Orifice equation Q=3P(h)^1.5 Weir equation where: A= free open area of grate P= weir perimeter h= feet of head (ponding depth) g= 32.2 feet per sec/sec Q=capacity of grate in CFS

Net total flow is the lower of the two equations except where the the ratio of the two solutions is between 0.667 and 1.5. In the latter case the net flow is 80% of the average of the two solutions as an approximation of transitional flow.

Inlet Capacities per IDOT Design Manual Neenah R-2504 TY D Grate

0.9 = Free open area of grate (sq. ft.)**6** = Weir Perimeter of grate (ft.)

	Capaci	ty Calculatio	on		
	Weir	Orifice	Net	Weir/Orifice	Flow Type
Ponding	Equation	Equation	Capacity	ratio	
0.05	0.20	0.97	0.20	0.21	Weir Flow
0.10	0.57	1.37	0.57	0.42	Weir Flow
0.15	1.05	1.68	1.05	0.62	Weir Flow
0.17	1.26	1.79	1.22	0.71	Transition Flow
0.20	1.61	1.94	1.42	0.83	Transition Flow
0.25	2.25	2.17	1.77	1.04	Transition Flow
0.30	2.96	2.37	2.13	1.25	Transition Flow
0.35	3.73	2.56	2.52	1.45	Transition Flow
0.40	4.55	2.74	2.74	1.66	Orifice Flow
0.45	5.43	2.91	2.91	1.87	Orifice Flow
0.50	6.36	3.06	3.06	2.08	Orifice Flow
0.55	7.34	3.21	3.21	2.28	Orifice Flow
0.60	8.37	3.36	3.36	2.49	Orifice Flow
0.65	9.43	3.49	3.49	2.70	Orifice Flow
0.70	10.54	3.63	3.63	2.91	Orifice Flow
0.75	11.69	3.75	3.75	3.12	Orifice Flow
0.82	13.37	3.92	3.92	3.41	
1.00	18.00	4.33	4.33	4.15	Orifice Flow
1.25	25.16	4.84	4.84	5.19	Orifice Flow
1.50	33.07	5.31	5.31	6.23	Orifice Flow
1.75	41.67	5.73	5.73	7.27	Orifice Flow
2.00	50.91	6.13	6.13	8.31	Orifice Flow
2.25	60.75	6.50	6.50	9.35	Orifice Flow
2.50	71.15	6.85	6.85	10.38	Orifice Flow
2.75	82.09	7.19	7.19	11.42	Orifice Flow
3.00	93.53	7.51	7.51	12.46	Orifice Flow
3.25	105.46	7.81	7.81	13.50	Orifice Flow
3.50	117.86	8.11	8.11	14.54	Orifice Flow
3.75	130.71	8.39	8.39	15.58	Orifice Flow
4.00	144.00	8.67	8.67	16.61	Orifice Flow
4.25	157.71	8.93	8.93	17.65	Orifice Flow
4.50	171.83	9.19	9.19	18.69	Orifice Flow

Notes:

Equations used Q=0.6A(2gh)^0.5 Orifice equation Q=3P(h)^1.5 Weir equation where: A= free open area of grate P= weir perimeter h= feet of head (ponding depth) g= 32.2 feet per sec/sec Q=capacity of grate in CFS

Net total flow is the lower of the two equations except where the the ratio of the two solutions is between 0.667 and 1.5. In the latter case the net flow is 80% of the average of the two solutions as an approximation of transitional flow.







Chick-fil-A 5200 Buffington Road Atlanta, Georgia 30349-2998



S C OQL **N** õ OGDEN \bigcirc

AVENUE - 60563 1163 E. OGDEN NAPERVILLE, II

FSR# 05590

REVISION SCHEDULENO.DATE

DESCRIPTION



ENGINEER'S PROJECT # 2302569 PRINTED FOR PRELIMINARY 10/16/2023 DRAWN BY: MRJ CHECKED BY: JFV Information contained on this drawing and in all digital files produced for above named project may not be reproduced in any manner without express written or verbal consent from authorized project representatives.

SHEET **EXISTING DETENTION** EXHIBIT



DATE



JOB: Chick-fil-A Naperville, IL JOB # 2302569

BY: NHL Date: 11/7/23

Elevation (ft)	Area (sq. ft.)	Area (acres)	Volume (ac-ft)	Cumulative Volume (ac-ft)	Cumulative Volume (cf)
764.32	1	0.00	0.00	0.000	0
765.00	1096	0.03	0.01	0.006	256
766.00	9324	0.21	0.10	0.110	4795

EXISTING SURFACE DETENTION







Chick-fil-A 5200 Buffington Road Atlanta, Georgia 30349-2998



SU J DQC **IRO** Q OGDEN

AVENUE - 60563 1163 E. OGDEN NAPERVILLE, II

FSR# 05590

REVISION SCHEDULENO.DATE

 \bigcirc

DESCRIPTION



2302569 PRELIMINARY 10/16/2023

DRAWN BY: MRJ CHECKED BY: JFV Information contained on this drawing and in all digital files produced for above named project may not be reproduced in any manner without express written or verbal consent from authorized project representatives.

ENGINEER'S PROJECT #

PRINTED FOR

DATE

SHEET EXISTING PIPE STORAGE EXHIBIT

SHEET NUMBER EPSE



STORM SEWER PIPE STORAGE VOLUME CALCULATIONS

Project # Project: Location	2302569 Chick-fi Napervi) II-A Nape IIe, IL	erville, IL			By Revised Checked	NHL	Date Date Date	11/7/2023		U/S	
				Тор					cu.ft.	Pipe Volume Filled at Elevation	Manhole	Manhole Volume (upstream of designated pipe) Filled at Elevation
Pipe #	Size	Length	US INV	Pipe	Slope	DS INV	Avg Inv	Pipe Area	Volume Full	766.00	Dia (ft)	766.00
1	16	138	760.34	761.67	0.06%	760.26	760.30	1.40	193	175	4	71
2	12	62	762.88	763.88	3.97%	760.42	761.65	0.79	49	44	5	61
3	15	63	760.47	761.72	0.21%	760.34	760.41	1.23	77	70	6	156

subtotal cu-ft 289

Total Pipe Volume Cu-Ft	319	290
Total Manhole Volume Cu-Ft		289
Provided Total Volume Cu-Ft		579
Provided Total Volume Ac-Ft		0.013
Maximum Water Elevation		766.00



STORM SEWER PIPE STORAGE VOLUME CALCULATIONS

Project # Project:	2302569 Chick-fi) I-A Nape IIe. II	rville, IL			By Revised Checked	NHL	Date Date Date	1/3/2024			
Loodion						onconcu		Dato			U/S	
				Тор					cu.ft.	Pipe Volume Filled at Elevation	Manhole	Manhole Volume (upstream of designated pipe) Filled at Elevation
Pipe #	Size	Length	US INV	Pipe	Slope	DS INV	Avg Inv	Pipe Area	Volume Full	766.00	Dia (ft)	766.00
ST-2	15	28	759.88	761.13	0.00%	759.88	759.88	1.23	34	34	4	77
ST-4	15	183	760.26	761.51	0.21%	759.88	760.07	1.23	225	204	4	72
ST-6	36	153	761.35	764.35	0.71%	760.26	760.81	7.07	1081	985	5	91
ST-10	36	70	762.00	765.00	0.93%	761.35	761.68	7.07	495	451	5	79
ST-12	24	79	762.60	764.60	0.76%	762.00	762.30	3.14	248	226	4	43
ST-20	12	21	761.20	762.20	4.48%	760.26	760.73	0.79	16	15	4	60
ST-22	15	33	759.95	761.20	0.21%	759.88	759.92	1.23	40	37	7	233
ST-24	36	174	760.32	763.32	0.21%	759.95	760.14	7.07	1230	1120	5	112
ST-26	36	54	760.43	763.43	0.20%	760.32	760.38	7.07	382	348	5	109
ST-28	30	58	760.55	763.05	0.21%	760.43	760.49	4.91	285	259	5	107
ST-31	15	2	762.88	764.13	4.00%	762.80	762.84	1.23	2	2	4	39
ST-33	36	60	760.15	763.15	0.33%	759.95	760.05	7.07	424	386	5	115
ST-35	36	71	761.30	764.30	1.62%	760.15	760.73	7.07	502	457	4	59

subtotal cu-ft 1196

Total Pipe Volume Cu-Ft	4965	4524
Total Manhole Volume Cu-Ft		1196
Provided Total Volume Cu-Ft		5720
Provided Total Volume Ac-Ft		0.131
Maximum Water Elevation		766.00

Hydraflow Storm Sewers Extension for Autodesk® Civil 3D® Plan



Storm Sewer IDF Curves

IDF file: IL B75 - NE.IDF



Hydraflow IDF Report

Return Period	Equation Coefficients (FHA)										
(Yrs)	В	D	E	(N/A)							
1	0.0000	0.0000	0.0000								
2	127.7602	21.7001	0.9991								
3	0.0000	0.0000	0.0000								
5	133.5045	19.5000	0.9578								
10	181.9707	20.8000	0.9836								
25	0.0000	0.0000	0.0000								
50	0.0000	0.0000	0.0000								
100	277.6214	20.1000	0.9656								
J:\2023\230256	9\ Design\Calc\Storm\Hydr a	Flow\IL B75 - NE.IDF									

Intensity = B / (Tc + D)^E

Return	Intensity Values (in/hr)												
(Yrs)	5 min	10	15	20	25	30	35	40	45	50	55	60	
1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
2	4.80	4.04	3.49	3.07	2.75	2.48	2.26	2.08	1.92	1.79	1.67	1.57	
3	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5	6.24	5.22	4.49	3.95	3.52	3.18	2.90	2.67	2.47	2.30	2.15	2.02	
10	7.44	6.25	5.39	4.74	4.23	3.82	3.48	3.20	2.96	2.76	2.58	2.42	
25	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
50	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
100	12.36	10.37	8.94	7.86	7.02	6.34	5.78	5.32	4.92	4.58	4.29	4.03	
Tc = time in mir	utes. Min Tc	= 5											

Storm Sewer Tabulation

Station Len Drng Area		Rnoff	Area x	С	Tc		Rain	Total	Cap	Vel	Pipe		Invert Ele	ev	HGL Ele	v	Grnd / Ri	m Elev	Line ID			
Line	To		Incr	Total	coen	Incr	Total	Inlet	Syst		now	run		Size	Slope	Dn	Up	Dn	Up	Dn	Up	
	Line	(ft)	(ac)	(ac)	(C)			(min)	(min)	(in/hr)	(cfs)	(cfs)	(ft/s)	(in)	(%)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	
1	End	28.000	0.14	2.46	0.95	0.13	2.10	5.0	23.0	2.9	14.44	0.00	11.77	15	0.00	759.88	759.88	761.13	762.53	761.21	765.76	ST-2
2	1	33.000	0.16	0.71	0.87	0.14	0.57	5.0	22.7	2.9	10.06	30.72	1.42	36	0.21	759.88	759.95	764.68	764.69	765.76	765.91	ST-22
3	2	174.000	0.18	0.23	0.85	0.15	0.20	5.0	5.7	4.7	9.36	30.75	1.32	36	0.21	759.95	760.32	764.72	764.75	765.91	767.16	ST-24
4	3	54.000	0.05	0.05	0.95	0.05	0.05	5.0	5.0	4.8	8.65	30.10	1.22	36	0.20	760.32	760.43	764.76	764.77	767.16	767.46	ST-26
5	4	58.000	0.00	0.00	0.00	0.00	0.00	0.0	0.0	0.0	8.42	18.65	1.72	30	0.21	760.43	760.55	764.79	764.81	767.46	767.20	ST-28
6	1	183.000	0.12	1.61	0.91	0.11	1.40	5.0	10.3	4.0	5.61	2.94	4.57	15	0.21	759.88	760.26	764.68	766.07	765.76	766.20	ST-4
7	6	153.000	0.06	1.34	0.89	0.05	1.16	5.0	6.9	4.5	5.18	56.29	0.73	36	0.71	760.26	761.35	766.39	766.40	766.20	767.11	ST-6
8	7	70.000	0.08	1.28	0.80	0.06	1.10	5.0	5.8	4.7	5.14	39.52	1.05	30	0.93	761.35	762.00	766.41	766.42	767.11	767.16	ST-10
9	8	79.000	0.22	1.20	0.94	0.21	1.04	5.0	5.0	4.8	4.99	19.71	1.59	24	0.76	762.00	762.60	766.43	766.47	767.16	767.21	ST-12
10	9	2.000	0.98	0.98	0.85	0.83	0.83	5.0	5.0	4.8	4.00	12.92	3.26	15	4.00	762.80	762.88	766.51	766.52	767.21	765.66	ST-31
11	6	23.000	0.15	0.15	0.89	0.13	0.13	5.0	5.0	4.8	0.64	13.05	0.52	15	4.09	760.26	761.20	766.39	766.39	766.20	766.81	ST-20
12	2	60.000	0.11	0.32	0.63	0.07	0.23	5.0	16.1	3.4	0.77	38.51	0.11	36	0.33	759.95	760.15	764.72	764.72	765.91	765.91	ST-33
13	12	71.000	0.21	0.21	0.75	0.16	0.16	5.0	5.0	4.8	0.76	84.88	0.11	36	1.62	760.15	761.30	764.72	764.72	765.91	766.56	ST-35
												24										
Proje		230256	s=Hydra	anow.str	1												or lines: 1	3		Kun Dai	ie. 1/4/202	24
NOT	ES:Inte	nsity = 1	27.76 /	(Inlet tim	ie + 21.7	0) ^ 1.00); Returr	n period	=Yrs. 2	; c = cir	e = ellip	b = bo	x									



Storm Sewer Profile





Storm Sewer Profile









BAR IS ONE INCH ON OFFICIAL DRAWINGS IF NOT ONE INCH, ADJUST SCALE ACCORDINGLY





Chick-fil-A 5200 Buffington Road Atlanta, Georgia 30349-2998



J DQL **N** õ OGDEN

AVENUE - 60563 1163 E. OGDEN NAPERVILLE, II

FSR# 05590

REVISION SCHEDULENO.DATE

DESCRIPTION



ENGINEER'S PROJECT # 2302569 PRELIMINARY 10/16/2023 DRAWN BY: MRJ CHECKED BY: JFV

Information contained on this drawing and in all digital files produced for above named project may not be reproduced in any manner without express written or verbal consent from authorized project representatives. SHEET EXISTING DRAINAGE

PLAN SHEET NUMBER



PRINTED FOR

DATE







Chick-fil-A 5200 Buffington Road Atlanta, Georgia 30349-2998



SU (JL C DQU **M** Š Ζ OGDEI \mathbf{C}

ENUE 563 AVE 60 1163 E. OGDEN NAPERVILLE, II

FSR# 05590

REVISION SCHEDULENO.DATE

DESCRIPTION



ENGINEER'S PROJECT #	2302569
PRINTED FOR	PRELIMINARY
DATE	10/16/2023
DRAWN BY: MRJ CHECKED BY: JFV	
Information contained on this drawing ar produced for above named project may any manner without express written or v authorized project representatives.	nd in all digital files not be reproduced in erbal consent from
SHEET	
PROPOSED DR PLAN	AINAGE
SHEET NUMBER	





LEGEND:



PROPOSED DRAINAGE AREA BOUNDARY ----- PROJECT AREA BOUNDARY DENOTES PROPOSED PERVIOUS AREA DRAINAGE ARROW





Chick-fil-A 5200 Buffington Road Atlanta, Georgia 30349-2998



IROQI õ OGDEN \mathbf{U}

AVENUE L 60563 1163 E. OGDEN NAPERVILLE, II

FSR# 05590

REVISION SCHEDULENO.DATE

DESCRIPTION



ENGINEER'S PF	ROJECT #	2302569
PRINTED FOR	PRE	LIMINARY
DATE	10	/16/2023
DRAWN BY: CHECKED BY:	MRJ JFV	
Information containe produced for above r any manner without authorized project re	d on this drawing and in all di named project may not be rep express written or verbal cons presentatives.	gital files produced in sent from
SHEET		
PROPO PLAN - (SED DRAIN OFF-SITE	AGE



GRADING & DRAINAGE NOTES

- CONTRACTOR IS RESPONSIBLE FOR COORDINATION OF SITE PLAN DOCUMENTS AND ARCHITECTURAL DESIGN FOR EXACT BUILDING UTILITY CONNECTION LOCATIONS, GREASE TRAP REQUIREMENTS/DETAILS, DOOR ACCESS, AND EXTERIOR GRADING. THE UTILITY SERVICE SIZES ARE TO BE DETERMINED BY THE ARCHITECT. THE CONTRACTOR SHALL COORDINATE INSTALLATION OF UTILITIES/SERVICES WITH THE INDIVIDUAL COMPANIES, TO AVOID CONFLICTS AND ENSURE PROPER DEPTHS ARE ACHIEVED. THE JURISDICTION UTILITY REQUIREMENTS SHALL ALSO BE MET, AS WELL AS COORDINATING THE UTILITY TIE-INS/CONNECTIONS PRIOR TO CONNECTING TO THE EXÍSTING UTILITY/SERVICE. WHERE CONFLICTS EXIST WITH THESE SITE PLANS, ENGINEER IS TO BE NOTIFIED PRIOR TO CONSTRUCTION TO RESOLVE SAME.
- SITE GRADING SHALL BE PERFORMED IN ACCORDANCE WITH THESE PLANS AND SPECIFICATIONS AND THE RECOMMENDATIONS SET FORTH IN THE GEOTECHNICAL REPORT. THE CONTRACTOR SHALL BE RESPONSIBLE FOR REMOVING AND REPLACING WITH SUITABLE MATERIALS AS SPECIFIED IN THE GEOTECHNICAL REPORT. ALL EXCAVATED OR FILLED AREAS SHALL BE COMPACTED AS OUTLINED IN THE GEOTECHNICAL REPORT. MOISTURE CONTENT AT TIME OF PLACEMENT SHALL BE SUBMITTED IN COMPACTION REPORT PREPARED BY A QUALIFIED GEOTECHNICAL ENGINEER, REGISTERED WITH THE STATE WHERE THE WORK IS PERFORMED, VERIFYING THAT ALL FILLED AREAS AND SUBGRADE AREAS WITHIN THE BUILDING PAD AREA AND AREAS TO BE PAVED HAVE BEEN COMPACTED IN ACCORDANCE WITH THESE PLANS AND SPECIFICATIONS AND THE RECOMMENDATIONS SET FORTH IN THE GEOTECHNICAL REPORT. SUBBASE MATERIAL FOR SIDEWALKS, CURB, OR ASPHALT SHALL BE FREE OF ORGANICS AND OTHER UNSUITABLE MATERIALS. SHOULD SUBBASE BE DEEMED UNSUITABLE BY OWNER OR OWNER'S REPRESENTATIVE, SUBBASE IS TO BE REMOVED AND FILLED WITH APPROVED FILL MATERIAL COMPACTED AS DIRECTED BY THE GEOTECHNICAL REPORT.
- ALL FILL, COMPACTION, AND BACKFILL MATERIALS REQUIRED FOR UTILITY INSTALLATION SHALL BE AS PER THE RECOMMENDATIONS PROVIDED IN THE GEOTECHNICAL REPORT AND SHALL BE COORDINATED WITH THE APPLICABLE UTILITY COMPANY SPECIFICATIONS.
- THE CONTRACTOR SHALL COMPLY TO THE FULLEST EXTENT WITH THE LATEST OSHA STANDARDS AND REGULATIONS, OR ANY OTHER AGENCY HAVING JURISDICTION FOR EXCAVATION AND TRENCHING PROCEDURES. THE CONTRACTOR IS RESPONSIBLE FOR DETERMINING THE "MEANS AND METHODS" REQUIRED TO MEET THE INTENT AND PERFORMANCE CRITERIA OF OSHA, AS WELL AS ANY OTHER ENTITY THAT HAS JURISDICTION FOR EXCAVATION AND/OR TRENCHING PROCEDURES.
- PAVEMENT SHALL BE SAW CUT IN STRAIGHT LINES TO THE FULL DEPTH OF THE EXISTING PAVEMENT. ALL DEBRIS FROM REMOVAL OPERATIONS SHALL BE REMOVED FROM THE SITE AT THE TIME OF EXCAVATION. STOCKPILING OF DEBRIS WILL NOT BE PERMITTED.
- THE TOPS OF EXISTING MANHOLES, INLET STRUCTURES, AND SANITARY CLEANOUT TOPS SHALL BE ADJUSTED, IF REQUIRED, TO MATCH PROPOSED GRADES IN ACCORDANCE WITH ALL APPLICABLE STANDARDS.
- THE CONTRACTOR IS RESPONSIBLE FOR VERIFICATION of existing topographic information and utili INVERT ELEVATIONS PRIOR TO COMMENCEMENT OF ANY CONSTRUCTION. CONTRACTOR TO ENSURE 0.75% MINIMUM SLOPE ALONG ALL ISLANDS, GUTTERS, AND CURBS: 1.0% ON ALL CONCRETE SURFACES; AND 1.5% MINIMUM ON ASPHALT, TO PREVENT PONDING. ANY DISCREPANCIES THAT MAY AFFECT THE PUBLIC SAFETY OR PROJECT COST MUST BE IDENTIFIED TO THE ENGINEER IN WRITING IMMEDIATELY. PROCEEDING WITH CONSTRUCTION WITHOUT NOTIFICATION IS DONE SO AT THE CONTRACTOR'S OWN RISK.
- PROPOSED TOP OF CURB ELEVATIONS ARE GENERALLY 6" ABOVE EXISTING LOCAL ASPHALT GRADE UNLESS OTHERWISE NOTED. FIELD ADJUST TO CREATE A MINIMUM OF 0.75% GUTTER GRADE ALONG CURB FACE. ENGINEER TO APPROVE FINAL CURBING CUT SHEETS PRIOR TO INSTALLATION.
- IN CASE OF DISCREPANCIES BETWEEN PLANS OR RELATIVE TO OTHER PLANS, THE SITE PLAN WILL TAKE PRECEDENCE. IMMEDIATELY NOTIFY THE ENGINEER IN WRITING OF ANY CONFLICTS.
- ONTRACTOR SHALL BE REQUIRED TO SECURE ALL NECESSARY PERMITS AND APPROVALS FOR ALL OFF-SITE MATERIAL SOURCES AND DISPOSAL FACILITIES. CONTRACTOR SHALL SUPPLY A COPY OF APPROVALS TO ENGINEER AND OWNER PRIOR TO INITIATING WORK.
- . SITE GRADING SHALL NOT PROCEED UNTIL EROSION CONTROL MEASURES HAVE BEEN INSTALLED.
- 2. SEE EROSION CONTROL PLAN FOR EROSION CONTROL MEASURES AND NOTES.
- 3. ALL EXISTING STRUCTURES, UNLESS OTHERWISE NOTED TO REMAIN, FENCING, TREES, & ETC., WITHIN CONSTRUCTION AREA SHALL BE REMOVED & DISPOSED OF OFF SITE. NO ON SITE BURNING WILL BE ALLOWED
- 14. ALL DRAINAGE STRUCTURES SHALL BE PRE-CAST.
- 15. ALL DRAINAGE STRUCTURES AND STORM SEWER PIPES SHALL MEET HEAVY DUTY TRAFFIC (H2O) LOADING AND BE INSTALLED ACCORDINGLY.
- 5. GENERAL CONTRACTOR SHALL NOTIFY ALL UTILITY COMPANIES HAVING UNDERGROUND UTILITIES ON SITE OR IN RIGHT-OF-WAY PRIOR TO EXCAVATION. CONTRACTOR SHALL CONTACT UTILITY LOCATING COMPANY AND LOCATE ALL UTILITIES PRIOR TO GRADING START.
- 7. NO PART OF THE PROPOSED PROJECT IS LOCATED WITHIN A FLOOD HAZARD AREA
- 8. SPOT ELEVATIONS SHOWN ARE @ EDGE OF PAVEMENT UNLESS OTHERWISE NOTED ON PLAN.
- 9. ALL CONCRETE CURB & GUTTER SHALL BE TYPE B-6.18 CURB UNLESS OTHERWISE NOTED ON THE PLANS.
- 20. ALL STORM SEWER JOINTS SHALL HAVE O-RING GASKETS.
- 21. MATCH EXISTING GRADES AT PROPERTY LINES AND/OR CONSTRUCTION LIMITS.

- DRAINAGE AWAY FROM BUILDINGS
- OF 1.5%.
- GRADED TO A MAXIMUM OF 1.5%
- PONDING OF PAVEMENT.
- OPERATIONS TO WITHIN CONSTRUCTION LIMITS AND AT THE SOLE RESPONSIBILITY OF THE CONTRACTOR.
- CONTROL TO THE CONSTRUCTION AREA AND HAUL ROADS TO PREVENT THE SPREAD OF DUST.
- 29. ALL FIELD TILES ENCOUNTERED SHALL BE REPLACED AND LOCATED AND IDENTIFIED ON THE RECORD PLANS BY THE CONTRACTOR.
- 30. ALL STORM DRAINAGE CONSTRUCTION SHALL BE PERFORMED IN ACCORDANCE WITH THE MOST CURRENT CITY OF NAPERVILLE STANDARDS AND SPECIFICATIONS.



Chick-fil-A 5200 Buffington Road Atlanta, Georgia 30349-2998

Q NU 63 \frown AV 60 2 Ø ш Ζ C 0

C 02 1163 NAPI

FSR# 05590

REVISION SCHEDULE NO. DATE

DESCRIPTION

ENGINEER'S PROJEC	T # 2302569
PRINTED FOR	PRELIMINARY
DATE	10/16/2023
DRAWN BY: MRJ CHECKED BY: JFV	
Information contained on this produced for above named p any manner without express authorized project representa	drawing and in all digital files roject may not be reproduced in written or verbal consent from tives.
SHEET	
GRADING	PLAN

SHEET NUMBER **C-300**

DEPARTMENT OF PUBLIC UTILITIES - ELECTRIC GENERAL NOTES:	ST-#	> <u>storm tags</u>			S-#	> <u>Sanitary</u> sewer
• THE DEVELOPER SHALL SUPPLY THE DPU-E ENGINEER WITH CATALOG CUTS FOR ALL CT/METER	ST-1	EXIST. FES RCP, 15"	ST-23	STM SWR CB 7' DIA., R-3235 TY A GRATE	S-1	EXIST. SAN SWR MH
EQUIPMENT (INCLUDING BUT NOT LIMITED TO METER SOCKETS, PT CABINET, CT CABINET, DISCONNECT CABINET) AND TRANSFORMER PAD/VAULT. THE CATALOG CUTS SHALL BE APPROVED		INV = 759.88		T/C = 765.91		EXIST. RIM = 765.88 PROP RIM = 765.60
BY DPU-E PRIOR TO PURCHASING.	ST-2	EXIST. 28 LIN FT SS RCP, 15"		$INV = 759.95 \text{ SW } 15^{\circ} \text{ RCP}$ $INV = 759.95 \text{ NW } 36^{\circ} \text{ RCP}$		INV = 761.48 NW 8"
THE CT/METER CABINET SHALL BE TOP FED. CT/METER FOURMENT ARE LONG LEAD TIME ITEMS AND DRILLE SHALL NOT RE HELD.		@ 0.00%		INV = 759.95 NE 36" RCP		INV = 761.48 E 8"
RESPONSIBLE FOR DELAYS RESULTING FROM NON-COMPLIANT CT/METER EQUIPMENT.						FXIST 103 LIN FT SAN SW
ELECTRICAL CONTRACTOR TBD.	51-3	EXIST. STM SWR CURB INLET T/C = 765.76	ST-24	174 LIN FT SS RCP, 36″	3-2	@ 0.70%
DPUE WILL PROVIDE, INSTALL, AND MAINTAIN THE TRANSFORMERS, ALL PRIMARY (15KV) CABLE AND CONDUIT, AND THE METERS AND INSTRUMENT TRANSFORMERS. DPUE WILL ALSO MAKE THE		INV = 759.88 E 15" RCP		© 0.21%		
FINAL CONNECTIONS IN THE TRANSFORMERS ONCE THE INSPECTION IS COMPLETE AND THE		INV = 759.88 NW 15" RCP	ST-25	STM SWR CB 5' DIA., R-3235 TY A GRATE	S-3	EXIST. SAN SWR MH
 BUILDING IS READY TO BE ENERGIZED. THE DEVELOPER IS RESPONSIBLE FOR PROVIDING, INSTALLING, AND MAINTAINING THE 		EVIST 187 LIN ET SS DCD 15"		T/C = 767.16		RIM = 766.59 INV = 762.20 W 8" VCP
TRANSFORMER PAD/VAULT, ALL SERVICE LATERAL (480V) CABLE AND CONDUIT, THE SERVICE	51-4	© 0.21%		$INV = 760.32 \text{ SW } 36^{\circ} \text{ RCP}$		INV = 762.30 NE 6" PVC
 ENTRANCE EQUIPMENT INCLUDING THE CT/METER CABINET AND ALL BANKED METER SOCKETS. THE DEVELOPER SHALL COORDINATE SITE CONSTRUCTION WITH DPU-E TO ALLOW ELECTRIC 						(CONTRACTOR TO VERFIY W
FACILITIES TO BE INSTALLED PRIOR PAVING AND CURBING. DPU-E REQUIRES 30 WORKING DAYS	ST-5	STM SWR CB 6' DIA., R-2504 TY D GRATE	ST-26	54 LIN FT SS RCP, 36"		TO ORDERING STRUCTURES
ADVANCE WRITTEN NOTICE PRIOR TO PAVEMENT INSTALLATION TO ALLOW FOR THE INSTALLATION OF ELECTRIC FACILITIES. GRADE ELEVATION MUST BE WITHIN 4" OF FINAL GRADING BEFORE		RIM = 766.20 INV = 760.26 W 15" RCP		© 0.21%		WITH ANT DISCRETANCIES.
ELECTRIC FACILITIES CAN BE INSTALLED.		$INV = 760.26 \text{ N} 15^{\circ} \text{ RCP}$	ST-27	STM SWR CB 5' DIA., R-3235 TY A GRATE	S-4	62 LIN FT SAN SWR, 6"F
 ELECTRIC FACILITIES SHALL BE INSTALLED PURSUANT TO SECTION 8-1C-3 OF THE CITY OF NAPERVILLE MUNICIPAL CODE. WHICH REQUIRES A CONSTRUCTION FEE PAYMENT FOR INSTALLATION 		INV = 760.26 E 36" RCP		T/C = 767.46		@ 1.04%
OF ELECTRIC FACILITIES.				INV = 760.43 SW 36" RCP	5 5	CLEANOUT (SEE DETAIL)
AT ALL TIMES, THE CUSTOMER SHALL BE SOLELY RESPONSIBLE FOR MAINTAINING A SUITABLE APPROACH TO THE METER LOCATION. WITH NO OBSTRUCTIONS WITHIN FOUR (4) FEET OF THE	SI-6	0 0 71%		INV = 760.43 E 30 RCP	5-5	RIM = 766.90
FRONT AND TWO (2) FEET OF THE SIDES OF THE METER. PER NAPERVILLE SERVICE RULES AND			ST-28	58 LIN FT SS RCP, 30"		INV = +/- 762.94
POLICIES 22.2.F. • CLEARANCE TO TRANSFORMER PAD SHALL RE 5 FEET FROM ALL SIDES 10 FEET FROM FROM	ST-7	6 LIN FT SS PVC CANOPY DRAIN, 6" SDR 26		© 0.21%		RO LINET CAN OUR ON T
AND THE AREA ABOVE MUST BE COMPLETELY CLEAR OF OBSTRUCTION. NO TREES, SHRUBS, OR		@ 1.00%	ST_20	STM SWR MH 5' DIA. R-1713 CL	S-6	00 LIN FI SAN SWR, 6" P @ 1 04%
OTHER OBSTACLES WILL BE ALLOWED WITHIN THIS AREA. TRANSFORMER PAD SHALL MAINTAIN MINIMUM CLEARANCE OF 20 FEET FROM EGRESS POINTS. PER DEUE SPECIFICATIONS 010-2130	ST-8	6 LIN FT SS PVC CANOPY DRAIN, 6" SDR 26	51 23	RIM = 767.20		INV @ S-4 = 762.92
AND C30-0016.		@ 1.00%		INV = 760.55 NW 15" RCP (EXISTING PIPE. CONTRACTOR		INV @ BLDG = 763.75
DPU-E REQUIRES A MINIMUM 5' OF SEPARATION BETWEEN ITS ELECTRIC FACILITIES AND ANY EIDE HYDRANTS STORM DRAINS STORM SEWERS WATER MAINS CAS MAINS FTC. THAT RUN				TO VERIFY EXISTING PIPE INVERT PRIOR TO ORDERING		(VERFIY W/ ARCH)
PARALLEL TO ITS FACILITIES.	ST-9	SIM SWR CB 5' DIA., R-3235 TY A GRATE T/C = 767.11		$INV = 760.55 \text{ W } 30^{\circ} \text{ RCP}$	\$_7	two-way clean out (see
TO HAVE AN EXISTING SERVICE DISCONNECTED CALL THE CITY DISPATCH OFFICE AT 630-420-6187 PLEASE ALLOW AT LEAST 24 HOURS NOTICE METERS AND METER SEALS ARE		INV = 761.35 W 36" RCP				RIM = 768.50
TO BE REMOVED ONLY BY DPU-E PERSONNEL. THE LOCATION AND TYPE OF NEW OR		INV = 761.35 NE 30" RCP	ST-30	EXIST. 149 LIN FT SS RCP, 15"		INV = +/- 763.73
REPLACEMENT METER RELATED EQUIPMENT MUST BE PRE-APPROVED IN WRITING BY DPU-E. AN ELECTRIC SERVICE MUST BE INSPECTED BY THE DEVELOPMENT SERVICES TEAM ELECTRICAL				© 0.15%		37 LIN ET SAN SWR 6" P
INSPECTOR PRIOR TO CONNECTION.	51-10	© 0.93%	ST-31	2 LIN FT SS RCP, 15"	3-0	@ 1.04%
APPROVAL OF METERING EQUIPMENT BY DPU-E DOES NOT REMOVE YOUR RESPONSIBILITY TO COMPLY WITH THE LATEST VERSION OF THE NATIONAL ELECTRICAL CODE AS ADOPTED BY THE				© 4.00%		INV @ S-4 = 762.76
CITY OF NAPERVILLE. DETERMINATION OF COMPLIANCE WITH THE NATIONAL ELECTRICAL CODE WILL	ST-11	STM SWR CB 5' DIA., R-3235 TY A GRATE	07 70			
 A CUSTOMER'S GROUNDING CONDUCTOR SHALL NOT BE CONNECTED TO DPU-E DISTRIBUTION 		I/C = 767.16	51-52	RIM = 765.66	5-9	RIM = 766.60
EQUIPMENT.		INV = 762.00 NW 24" RCP		INV = 762.88 W 15" RCP		INV = +/- 763.09
 DUE TO SUPPLY CHAIN ISSUES DPU-E IS EXPERIENCING LONG LEAD TIMES (+400 DAYS) ON TRANSFORMERS. PLEASE TAKE THIS INTO CONSIDERATION WHEN PLANNING CONSTRUCTION. 			ot	COLUN ET SS DOD ZC"		
• PLEASE IDENTIFY PREFERRED VOLTAGE LEVEL. 1-PHASE 120/240, 1-PHASE 120/208, 3-PHASE	ST-12	79 LIN FT SS RCP, 24"	51-33	@ 0.33%	S-10	GREASE TRAP (1,000 GAL.)
120/208V OR, 3-PHASE 277/480V? PLEASE COMPLETED A SERVICE LOADING SPREADSHEET FOR		@ 0.76%				RIM(S) = 767.15 E, 767.1
• THE DEVELOPER IS RESPONSIBLE FOR THE CONSTRUCTION AND INSTALLATION OF A TRANSFORMER	ST-13	STM SWR CB 4' DIA., R-3235 TY A GRATE	ST-34	STM SWR CB 5' DIA., R-3235 TY A GRATE		INV = 763.30 (INLET)
PAD AND VAULT. THE DPU-E ENGINEER MUST BE INFORMED PRIOR TO THE INSTALLATION OF THE AND VAULT. A MAIN DISCONNECT OR CIRCUIT BREAKER IS REQUIRED FOR DPU-E ACCESS		T/C = 767.21		1/C = 765.91		INV = 763.13 (OUTLET)
IN CASE OF A NEED FOR SERVICE OR IN AN EMERGENCY. DPU-E SHALL MAKE THE FINAL		INV = 762.60 SE 24'' RCP INV = 762.60 W 8'' RCP		INV = 760.15 Ke 36" Ker INV = 760.15 SE 36" RCP	S-11	44 LIN FT SAN SWR, 6"F
CONNECTIONS OF THE CUSTOMER'S SERVICE TO THE TRANSFORMER TERMINALS. A MINIMUM OF FIGHT FEFT OF ADDITIONAL CONDUCTOR LENGTH MUST BE LEFT ON THE CUSTOMER'S SERVICE		INV = 762.80 NE 15" RCP				@ 1.04%
CABLES.			ST-35	71 LIN FT SS RCP, 36"		INV $@$ BLDG = 763.75
	ST-14	88 LIN FT SS PVC, 8" SDR 26		@ 1.62%		(VERFIY W/ ARCH)
		© 1.00%	ST-36	STM SWR CB 4' DIA., R-3235 TY A GRATE	S-12	TWO-WAY CLEAN OUT (SEE
	ST-15	23 LIN FT SS PVC ROOF DRAIN, 8" SDR 26		T/C = 766.56		RIM = 768.50
		@ 1.00%		INV - /01.3U SW 30 KCP		INV = +/- 763.73
	ST-16	23 LIN FT SS PVC ROOF DRAIN, 8" SDR 26	ST-37	135 LIN FT SS RCP, 15"		
		@ 1.00%		© 0.17%		
		7 LIN ET SS DVG GANGRY DRAWL S" ODD SS		(PIPE TO BE REMOVED & REPLACED - MATCH		
	ST-17	/ LIN FI SS FVL CANUFY DRAIN, 6" SDR 26 @ 1.00%		EXISTING PIPE INVERTS)		
	ST-18	7 LIN FT SS PVC CANOPY DRAIN, 6" SDR 26				
		@ 1.00%				
	ST-19	7 LIN FT SS PVC CANOPY DRAIN, 6" SDR 26				
		@ 1.00%				
	ST-20	23 LIN FT SS RCP, 15"				
		@ 4.09%				
	ST-21	SIM SWR CB 4′ DIA., R-3235 TY A GRATE T/C = 766.81				
		INV = 761.20 SE 15" RCP				
	ST-22	33 LIN FT SS RCP, 15"		NOTE:		
		@ 0.21%		* ALL STORM STRUCTURES WITHIN PAVED AREAS REQUIRE WEEP HOLES. SEE		
				DETAIL 10 ON SHEET C-403 FOR WEEP HOLE DETAILS.		

<u>r tags</u>	A CONFLICT TAGS
	* OMITTED FOR THIS SUBMITTAL
SWR MAIN, 8" VCP	
C (TO BE CORED)	
S. NOTIFY ENGINEER	
PVC (SDR 26)	
PVC (SDR 26)	
EE DETAIL)	
PVC (SDR 26)	
EE DETAIL)	
) Plan for details	
.15 W	
PVC (SDR 26)	
EE DETAIL)	

Chick-fil-A 5200 Buffington Road Atlanta, Georgia 30349-2998

S J 0 OGDEN & IROQU 1163 E. OGDEN AVENUE NAPERVILLE, IL 60563 IROQU X CH

FSR# 05590

REVISION SCHEDULENO.DATE

DESCRIPTION

P R E L I M I N A R Y NOT FOR CONSTRUCTION

ENGINEER'S PROJECT #	2302569								
PRINTED FOR	PRELIMINARY								
DATE	10/16/2023								
DRAWN BY: MRJ CHECKED BY: JFV									
Information contained on this drawing and in all digital files produced for above named project may not be reproduced in any manner without express written or verbal consent from authorized project representatives.									
SHEET UTILITY TAGS									

SHEET NUMBER

and the second second

• •--

and the second second

and the second second

RUNOFF COEFFICIENTS

TYPE OF DRAINAGE AREA SURFACESMIN.MAX.ROOFS, slag to metal0.750.95Asphalt0.700.95Concrete0.800.95Gravel, from clean and loose to clay and loose to well graded, some clay on siltBare0.100.40EARTH SURFACESSand, from uniform grain size, no silt or clay end loor silt contentBare0.200.60Loarn, from sandy or gravelly to clay be high clay or silt contentBare0.250.65Dense Vegetation0.150.500.50Dense Vegetation0.150.500.60Dense Vegetation0.150		RUN COEFFIC	off Cient <i>C</i>		
ROOFS, slag to metal 0.75 0.96 Asphalt 0.70 0.995 Concrete 0.80 0.95 Gravel, from clean and loose to clayer and compact 0.25 0.70 R. R. YARDS 0.20 0.40 Sand, from uniform grain size, no fines to well graded, some clay or silt Bare 0.15 0.50 Light Vegetation 0.10 0.40 0.40 Dense Vegetation 0.05 0.30 Gravel, from sandy or gravelly to clayer Bare 0.20 0.60 Light Vegetation 0.10 0.45 0.35 Gravel, from clean gravel and gravel sand mixtures, no silt or clay to high clay or silt content Bare 0.25 0.65 Bare 0.30 0.75 0.40 0.40 0.40 SURFACES Clay, from coarse sandy or silt or clay to high clay or silt content Bare 0.30 0.75 Light Vegetation 0.15 0.50 0.60 0.60 0.50 pure colloidal clays City, business areas 0.70 0.95 0		MIN.	MAX.		
PAVEMENTSAsphalt0.700.95Concrete0.800.95Gravel, from clean and loose to clay uniform grain size, no fines to well graded, some clay or sitBare0.150.50Sand, from uniform grain size, no fines to well graded, some clay or sitBare0.100.40Loam, from sandy or gravelly to clay eyBare0.200.60Light Vegetation0.100.45Dense Vegetation0.050.30Gravel, from clean gravel and gravel sand mixtures, no silt or 	ROOFS, slag to	metal		0.75	0.95
PAVEMENTSConcrete0.800.95Gravel, from clean and loose to clayey and compact0.250.70R. R. YARDS0.200.40Sand, from uniform grain size, no fines to well graded, some clay or siltBare0.150.50Light Vegetation0.050.30Bare0.200.60Light Vegetation0.050.30CayeyDense Vegetation0.050.35Gravel, from clean gravel and gravel sand mixtures, no silt or clay to high clay or silt contentBare0.250.65Light Vegetation0.150.500.35Dense Vegetation0.150.500.35Dense Vegetation0.150.500.35Clay, from coarse sandy or silt or clay to high clay or silt contentBare0.300.75Light Vegetation0.100.400.400.40Dense Vegetation0.100.400.40Dense Vegetation0.100.400.50Dense Vegetation0.100.500.60Dense Vegetation0.100.400.50Dense Vegetation0.100.500.60Dense Vegetation0.100.500.60Dense Vegetation0.100.550.55Rural districts, vary as to soil & vegetation0.100.25Vegetation0.100.250.55Rural districts, vary as to soil & vegetation0.100.25Parks, Golf Courses, etc., vary as to soil & vegetation0.100.5			0.70	0.95	
Bare 0.25 0.70 Loam, from sandy or gravelly to silt Bare 0.15 0.50 Loam, from sandy or gravelly to clayey Bare 0.20 0.40 Loam, from sandy or gravelly to clayey Bare 0.20 0.40 Bare 0.20 0.40 0.40 Loam, from sandy or gravelly to clayey Bare 0.20 0.60 Loam, from clean gravel and gravel sand mixtures, no silt or clay to high clay or silt content Bare 0.25 0.65 Light Vegetation 0.15 0.50 0.35 0.50 0.35 Bare 0.25 0.65 0.35 0.50 0.50 0.50 SURFACES Gravel, from coarse sandy or silt or pure colloidal clays Bare 0.20 0.60 0.50 0.50 Clay, from coarse sandy or silty to pure colloidal clays Dense Vegetation 0.15 0.50 0.50 City, business areas City, dense residential areas, vary as to soil & vegetation 0.15 0.55 0.55 Rural districts, vary as to soil & vegetation 0.10 0.25 0.10 </td <td>PAVEMENTS</td> <td>Concrete</td> <td></td> <td>0.80</td> <td>0.95</td>	PAVEMENTS	Concrete		0.80	0.95
R. R. YARDS 0.20 0.40 Sand, from uniform grain size, no fines to well graded, some clay or silt Bare 0.10 0.40 Light Vegetation 0.10 0.40 Dense Vegetation 0.05 0.30 Bare 0.20 0.60 Light Vegetation 0.10 0.40 Loam, from sandy or gravelly to clayey Bare 0.20 0.60 0.35 Gravel, from clean gravel and gravel sand mixtures, no silt or clay to high clay or silt content Bare 0.25 0.65 SURFACES Clay, from coarse sandy or silty to pure colloidal clays Bare 0.20 0.60 Dense Vegetation 0.15 0.50 0.50 0.40 Bare 0.20 0.60 Dense Vegetation 0.10 0.40 Bare 0.30 0.75 Light Vegetation 0.10 0.40 Bare 0.30 0.75 Light Vegetation 0.20 0.60 Dense Vegetation 0.15 0.50 0.50 0.50 0.50 Cotty, business areas 0.70 0.95		Gravel, from clean and loose to clay	ey and compact	0.25	0.70
EARTH Sand, from uniform grain size, no fines to well graded, some clay or silt Bare 0.10 0.40 Light Vegetation 0.05 0.30 Bare 0.20 0.60 Loam, from sandy or gravelly to clayey Bare 0.20 0.60 Gravel, from clean gravel and gravel sand mixtures, no silt or clay to high clay or silt content Bare 0.25 0.65 Light Vegetation 0.10 0.44 0.40 0.40 0.40 SURFACES Gravel, from clean gravel and gravel sand mixtures, no silt or clay to high clay or silt content Bare 0.25 0.65 Light Vegetation 0.10 0.40 0.40 0.40 0.40 Bare 0.30 0.75 0.50 0.50 0.50 Clay, from coarse sandy or silty to pure colloidal clays Bare 0.30 0.75 0.50 City, business areas 0.70 0.95 0.50 0.50 0.60 Dense Vegetation 0.10 0.25 0.55 0.55 0.55 Rural districts, vary as to soil & vegetation 0.10 0.25	R. R. YARDS		_	0.20	0.40
EARTH SURFACES City, business areas City, business areas City, business areas City, dense residential areas, vary as to soil & vegetation 0.10 0.40 COMPOSITE AREAS Suburban residential areas, vary as to soil & vegetation 0.05 0.30 Light Vegetation 0.10 0.40 Dense Vegetation 0.05 0.30 Bare 0.20 0.60 Light Vegetation 0.10 0.45 Dense Vegetation 0.10 0.45 Dense Vegetation 0.05 0.35 Bare 0.25 0.65 Light Vegetation 0.15 0.50 Dense Vegetation 0.10 0.40 Bare 0.30 0.75 Light Vegetation 0.10 0.40 Bare 0.30 0.75 Light Vegetation 0.10 0.40 Dense Vegetation 0.10 0.40 Dense Vegetation 0.15 0.50 Dense Vegetation 0.10 0.50 Dense Vegetation 0.10 0.50 <td></td> <td>Sand from uniform grain size no</td> <td>Bare</td> <td>0.15</td> <td>0.50</td>		Sand from uniform grain size no	Bare	0.15	0.50
silt Dense Vegetation 0.05 0.30 Bare 0.20 0.60 1 1 0.45 0.60 Loam, from sandy or gravelly to clayey Gravel, from clean gravel and gravel sand mixtures, no silt or clay to high clay or silt content 1 0.10 0.45 0.65 1 0.50 0.35 0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.65 1 1 0.40 0.50 0.60 0.60 0.40 0.50 0.50 0.50 0.50 0.50 0.50 0.50		fines to well graded, some clay or	Light Vegetation	0.10	0.40
EARTH SURFACESLoam, from sandy or gravelly to clayeyBare0.200.60Gravel, from clean gravel and gravel sand mixtures, no silt or clay to high clay or silt contentBare0.250.65Light Vegetation0.150.500.450.60Dense Vegetation0.150.500.60Dense Vegetation0.100.40Bare0.300.75Clay, from coarse sandy or silty to pure colloidal claysBare0.300.75City, business areas0.700.950.65City, dense residential areas, vary as to soil & vegetation0.150.50Suburban residential areas, vary as to soil & vegetation0.350.55Rural districts, vary as to soil & vegetation0.350.55Rural districts, vary as to soil & vegetation0.100.25Parks, Golf Courses, etc., vary as to soil & vegetation0.100.35Sandy soil, flat 2%0.150.100.15Aury soil, flat 2%0.130.170.13Heavy soil, flat 2%0.180.22Heavy soil, steep, 7%0.180.22Heavy soil, steep 7%0.350.35		silt	Dense Vegetation	0.05	0.30
Loam, from sandy or gravelly to clayey Light Vegetation 0.10 0.45 Gravel, from clean gravel and gravel sand mixtures, no silt or clay to high clay or silt content Bare 0.25 0.65 Light Vegetation 0.10 0.46 0.05 0.35 SURFACES Gravel, from clean gravel and gravel sand mixtures, no silt or clay to high clay or silt content Bare 0.25 0.65 Light Vegetation 0.10 0.40 0.40 0.10 0.40 Dense Vegetation 0.10 0.40 0.10 0.40 Dense Vegetation 0.10 0.40 0.40 Dense Vegetation 0.10 0.40 0.40 Dense Vegetation 0.20 0.60 0.60 Dense Vegetation 0.15 0.50 0.65 City, business areas 0.70 0.95 0.65 City, dense residential areas, vary as to soil & vegetation 0.35 0.55 Rural districts, vary as to soil & vegetation 0.10 0.35 0.55 Rural districts, vary as to soil & vegetation 0.10 0.15 0.20 <td></td> <td></td> <td>Bare</td> <td>0.20</td> <td>0.60</td>			Bare	0.20	0.60
EARTH SURFACES Clayey Gravel, from clean gravel and gravel sand mixtures, no silt or clay to high clay or silt content Dense Vegetation 0.05 0.35 Bare 0.25 0.65 0.65 Light Vegetation 0.10 0.40 Dense Vegetation 0.20 0.60 Dense Vegetation 0.20 0.60 Dense Vegetation 0.15 0.50 City, business areas 0.70 0.95 City, dense residential areas, vary as to soil & vegetation 0.10 0.65 Vegetation 0.10 0.25 0.55 Rural districts, vary as to soil & vegetation 0.10 0.25 Parks, Golf Courses, etc., vary as to soil & vegetation 0.10 0.15 Sandy soil, flat 2% 0.10 0.15 0.20 Heavy soil, daverage 2% to 7% 0.18 <td></td> <td>Loom from condu or grouplly to</td> <td>Light Vegetation</td> <td>0.10</td> <td>0.45</td>		Loom from condu or grouplly to	Light Vegetation	0.10	0.45
Gravel, from clean gravel and gravel sand mixtures, no silt or clay to high clay or silt contentBare0.250.65Light Vegetation0.100.40Dense Vegetation0.100.40Dense Vegetation0.200.60pure colloidal claysDense Vegetation0.200.60Dense Vegetation0.150.500.60Dense Vegetation0.150.500.60pure colloidal claysDense Vegetation0.150.50City, business areas0.700.950.65City, dense residential areas, vary as to soil & vegetation0.600.65vegetation0.500.650.65Rural districts, vary as to soil & vegetation0.100.25Parks, Golf Courses, etc., vary as to soil & vegetation0.100.35Sandy soil, flat 2%0.150.100.15Sandy soil, steep, 7%0.130.17Heavy soil, flat 2%0.130.17Heavy soil, steep 7%0.250.35		clayey	Dense Vegetation	0.05	0.35
EARTH SURFACESgravel sand mixtures, no silt or clay to high clay or silt contentLight Vegetation0.150.50Bare0.300.75Clay, from coarse sandy or silty to pure colloidal claysBare0.300.75Light Vegetation0.200.60Dense Vegetation0.150.50City, business areas0.700.95City, dense residential areas, vary as to soil & vegetation0.700.95City, dense residential areas, vary as to soil & vegetation0.100.25Suburban residential areas, vary as to soil & vegetation0.100.25Rural districts, vary as to soil & vegetation0.100.25Parks, Golf Courses, etc., vary as to soil & vegetation0.100.35Sandy soil, flat 2%0.100.150.20Sandy soil, steep, 7%0.150.20Heavy soil, flat 2%0.130.17Heavy soil, steep, 7%0.180.22Heavy soil, steep 7%0.250.35		Gravel, from clean gravel and	Bare	0.25	0.65
LARTH SURFACESClay to high clay of silt contentDense Vegetation0.100.40SURFACESClay, from coarse sandy or silty to pure colloidal claysBare0.300.75Light Vegetation0.200.60Dense Vegetation0.150.50Light Vegetation0.150.50City, business areas0.700.95City, dense residential areas, vary as to soil & vegetation0.500.65Suburban residential areas, vary as to soil & vegetation0.350.55Rural districts, vary as to soil & vegetation0.100.25Parks, Golf Courses, etc., vary as to soil & vegetation0.100.35Sandy soil, flat 2%0.100.150.20LAWNSSandy soil, steep, 7%0.130.17Heavy soil, flat 2%0.130.170.18Heavy soil, steep 7%0.180.220.35	ЕЛДТЦ	gravel sand mixtures, no silt or	Light Vegetation	0.15	0.50
Clay, from coarse sandy or silty to pure colloidal claysBare0.300.75Light Vegetation0.200.60Dense Vegetation0.150.50Dense Vegetation0.150.50City, business areas0.700.95City, dense residential areas, vary as to soil & vegetation0.500.65Suburban residential areas, vary as to soil & vegetation0.350.55Rural districts, vary as to soil & vegetation0.100.25Parks, Golf Courses, etc., vary as to soil & vegetation0.100.35Sandy soil, flat 2%0.100.15Sandy soil, steep, 7%0.130.17Heavy soil, flat 2%0.130.17Heavy soil, flat 2%0.250.35Heavy soil, steep 7%0.250.35Heavy soil,	SURFACES	ciay to high ciay of silt content	Dense Vegetation	0.10	0.40
Clay, from coarse sandy or silty to pure colloidal clays Light Vegetation 0.20 0.60 Dense Vegetation 0.15 0.50 City, business areas 0.70 0.95 City, dense residential areas, vary as to soil & 0.50 0.65 City, dense residential areas, vary as to soil & vegetation 0.35 0.55 Suburban residential areas, vary as to soil & vegetation 0.10 0.25 Rural districts, vary as to soil & vegetation 0.10 0.35 Parks, Golf Courses, etc., vary as to soil & vegetation 0.10 0.35 Sandy soil, flat 2% 0.05 0.10 0.15 Sandy soil, steep, 7% 0.13 0.17 Heavy soil, flat 2% 0.13 0.17 Heavy soil, average 2% to 7% 0.18 0.22			Bare	0.30	0.75
Dense Vegetation0.150.50Dense Vegetation0.700.95City, business areas0.700.95City, dense residential areas, vary as to soil & vegetation0.500.65Suburban residential areas, vary as to soil & vegetation0.350.55Rural districts, vary as to soil & vegetation0.100.25Parks, Golf Courses, etc., vary as to soil & vegetation0.100.35Sandy soil, flat 2%0.050.100.15Sandy soil, steep, 7%0.100.150.20Heavy soil, flat 2%0.130.170.18Heavy soil, average, 2% to 7%0.180.220.25Heavy soil, steep 7%0.180.220.25		Clay, from coarse sandy or silty to	Light Vegetation	0.20	0.60
City, business areas0.700.95City, dense residential areas, vary as to soil & vegetation0.500.65Suburban residential areas, vary as to soil & vegetation0.350.55Rural districts, vary as to soil & vegetation0.100.25Parks, Golf Courses, etc., vary as to soil & vegetation0.100.35Sandy soil, flat 2%0.050.10Sandy soil, average 2% to 7%0.100.15Sandy soil, steep, 7%0.150.20Heavy soil, flat 2%0.130.17Heavy soil, steep, 7%0.180.22Heavy soil, steep 7%0.180.22		pure conoidal clays	Dense Vegetation	0.15	0.50
COMPOSITE AREASCity, dense residential areas, vary as to soil & vegetation0.500.65Suburban residential areas, vary as to soil & vegetation0.350.55Rural districts, vary as to soil & vegetation0.100.25Parks, Golf Courses, etc., vary as to soil & vegetation0.100.35Sandy soil, flat 2%0.050.10Sandy soil, average 2% to 7%0.100.15Sandy soil, steep, 7%0.130.17Heavy soil, flat 2%0.180.22Heavy soil, steep 7%0.180.22		City, business areas		0.70	0.95
COMPOSITE AREASSuburban residential areas, vary as to soil & vegetation0.350.55Rural districts, vary as to soil & vegetation0.100.25Parks, Golf Courses, etc., vary as to soil & vegetation0.100.35Parks, Golf Courses, etc., vary as to soil & vegetation0.100.35Sandy soil, flat 2%0.050.10Sandy soil, average 2% to 7%0.100.15Sandy soil, steep, 7%0.150.20Heavy soil, flat 2%0.130.17Heavy soil, steep 7%0.180.22Heavy soil, steep 7%0.180.22		City, dense residential areas, vary a vegetation	0.50	0.65	
AREAS Rural districts, vary as to soil & vegetation 0.10 0.25 Parks, Golf Courses, etc., vary as to soil & vegetation 0.10 0.35 Parks, Golf Courses, etc., vary as to soil & vegetation 0.10 0.35 Sandy soil, flat 2% 0.05 0.10 Sandy soil, average 2% to 7% 0.10 0.15 Sandy soil, steep, 7% 0.15 0.20 Heavy soil, flat 2% 0.13 0.17 Heavy soil, average, 2% to 7% 0.18 0.22 Heavy soil, steep 7% 0.25 0.35	COMPOSITE	Suburban residential areas, vary as	0.35	0.55	
Parks, Golf Courses, etc., vary as to soil & vegetation 0.10 0.35 Sandy soil, flat 2% 0.05 0.10 Sandy soil, average 2% to 7% 0.10 0.15 Sandy soil, steep, 7% 0.15 0.20 Heavy soil, flat 2% 0.13 0.17 Heavy soil, average, 2% to 7% 0.18 0.22 Heavy soil, steep 7% 0.25 0.35	AREAS	Rural districts, vary as to soil & vege	0.10	0.25	
Sandy soil, flat 2% 0.05 0.10 Sandy soil, average 2% to 7% 0.10 0.15 Sandy soil, steep, 7% 0.15 0.20 Heavy soil, flat 2% 0.13 0.17 Heavy soil, average, 2% to 7% 0.18 0.22 Heavy soil, steep 7% 0.25 0.35		Parks, Golf Courses, etc., vary as to	0.10	0.35	
Sandy soil, average 2% to 7% 0.10 0.15 Sandy soil, steep, 7% 0.15 0.20 Heavy soil, flat 2% 0.13 0.17 Heavy soil, average, 2% to 7% 0.18 0.22 Heavy soil, steep 7% 0.25 0.35		Sandy soil, flat 2%	0.05	0.10	
LAWNS Sandy soil, steep, 7% 0.15 0.20 Heavy soil, flat 2% 0.13 0.17 Heavy soil, average, 2% to 7% 0.18 0.22 Heavy soil, steep 7% 0.25 0.35		Sandy soil, average 2% to 7%	0.10	0.15	
LAWNS Heavy soil, flat 2% 0.13 0.17 Heavy soil, average, 2% to 7% 0.18 0.22 Heavy soil, steep 7% 0.25 0.35		Sandy soil, steep, 7%	0.15	0.20	
Heavy soil, average, 2% to 7% 0.18 0.22 Heavy soil, steep 7% 0.25 0.35	LAWNS	Heavy soil, flat 2%		0.13	0.17
Heavy soil, steep 7% 0.25 0.35		Heavy soil, average, 2% to 7%		0.18	0.22
		Heavy soil, steep 7%		0.25	0.35

Note: Values of C for earth surfaces are further varied by degree of saturation, compaction, surface irregularity and slope, by character of subsoil, and by presence of frost or glazed snow or ice.

Figure 2. Climatic sections used in developing Illinois frequency estimates

Storm	2-	3-	4-	6-	9-	1-	2-	5-	10-	25-	50-	100-	500-
Duration	month	month	month	month	month	year	year	year	year	year	year	year	year
5 minutes	0.19	0.22	0.24	0.27	0.31	0.33	0.40	0.52	0.62	0.77	0.90	1.03	1.35
10 minutes	0.33	0.38	0.41	0.47	0.53	0.58	0.70	0.90	1.08	1.35	1.58	1.80	2.36
15 minutes	0.42	0.49	0.53	0.61	0.69	0.75	0.90	1.16	1.39	1.74	2.03	2.32	3.04
30 minutes	0.58	0.66	0.73	0.83	0.94	1.03	1.24	1.59	1.91	2.39	2.78	3.17	4.16
1 hour	0.74	0.84	0.93	1.05	1.20	1.30	1.57	2.02	2.42	3.03	3.53	4.03	5.28
2 hours	0.91	1.04	1.14	1.30	1.48	1.61	1.94	2.49	2.99	3.74	4.35	4.97	6.52
3 hours	1.00	1.15	1.26	1.44	1.63	1.77	2.14	2.75	3.30	4.13	4.80	5.49	7.20
6 hours	1.18	1.35	1.48	1.68	1.91	2.08	2.51	3.23	3.86	4.84	5.63	6.43	8.43
12 hours	1.37	1.56	1.71	1.95	2.21	2.41	2.91	3.74	4.48	5.61	6.53	7.46	9.78
18 hours	1.48	1.69	1.85	2.11	2.39	2.61	3.14	4.04	4.84	6.06	7.05	8.06	10.57
24 hours	1.57	1.80	1.97	2.24	2.55	2.77	3.34	4.30	5.15	6.45	7.50	8.57	11.24
48 hours	1.72	1.97	2.16	2.46	2.79	3.04	3.66	4.71	5.62	6.99	8.13	9.28	12.10
72 hours	1.87	2.14	2.34	2.67	3.03	3.30	3.97	5.08	6.05	7.49	8.64	9.85	12.81
120 hours	2.08	2.38	2.61	2.97	3.37	3.67	4.42	5.63	6.68	8.16	9.39	10.66	13.81
240 hours	2.63	3.01	3.30	3.76	4.27	4.65	5.60	7.09	8.25	9.90	11.26	12.65	16.00

Table 7. Rainfall (inches) for Given Recurrence Interval for Section 2 (Northeast)